EMI Detection and Classification of Underwater Munitions:

Sequim Bay Demonstration

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Terrestrial vs Marine EMI classification





Physical Model

Dipole model effective for classification

Background Signals

Low background levels Some challenges in magnetic geology

Instrument Positioning

Dynamic: RTK-GPS, SLAM, RTS

Cued: Static and fixed geometry

Target Signal Strength

Close proximity to targets: High SNR











Terrestrial vs Marine EMI classification

Physical Model

Potential interaction effects between object and sea-water (early time)

Background Signals

Varies with water depth and temperature, sensor height, sediment composition

Instrument Positioning

Dynamic: Underwater positioning is much less accurate

Cued: Logistical challenges

Target Signal Strength

Offset to the sea-bottom: Low SNR













Outline

- Modeling & characterizing EMI response in a marine setting
 - Integral equation (IE) to compute conductive layered background and target responses
 - Conductive background response removal
 - Validation of magnetic dipole model
- Mitigating sensor positional uncertainties
 - Independent model location inversion (IMLI)
- Enhancing target detectability
 - TEM synthetic aperture (SA) method
- Results of Sequim Bay







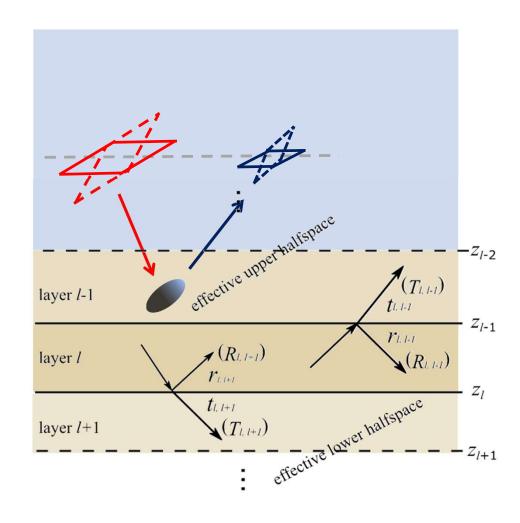






Modeling & Characterizing EMI Response in a Marine Setting

- Developed an integral equation technique that computes the EMI response for an arbitrarily oriented sensor in a multi-layered medium
- Technique also used to calculate scattering response of an elongated target in a layered medium
- Implementation: apply appropriate source and field decomposition and defining generalized reflection and transmission coefficients at interfaces (Recursive Propagation)



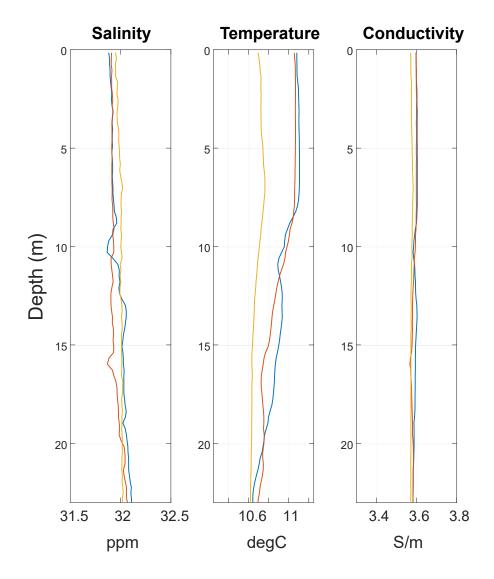




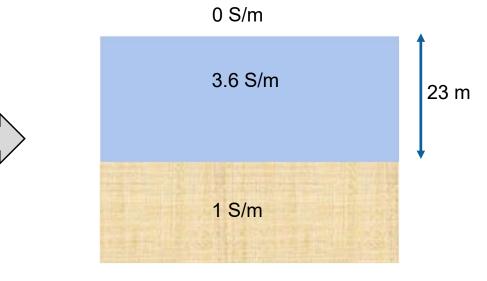


Estimating EMI Background Responses

CTD Cast Data



- 2021 data acquisition at Sequim Bay
- A 3-layer model is constructed assuming homogenous sea-water and sea-bed conductivity



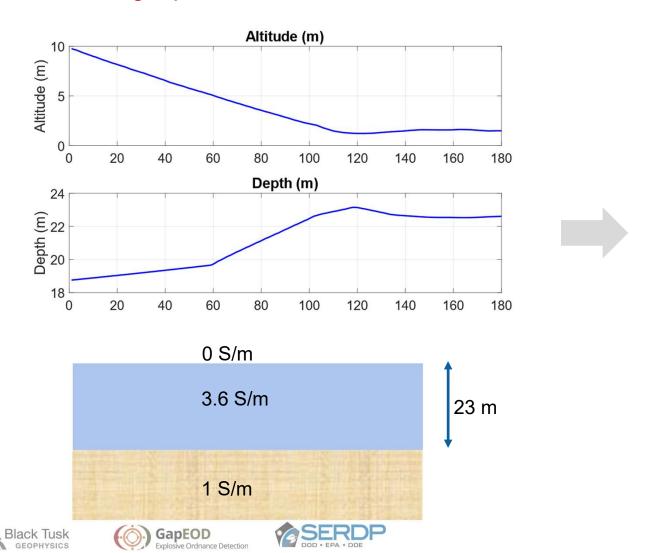




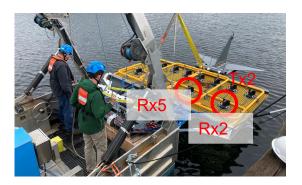


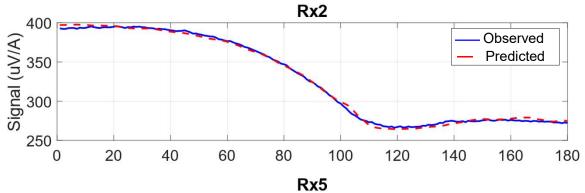
Estimating EMI Background Responses

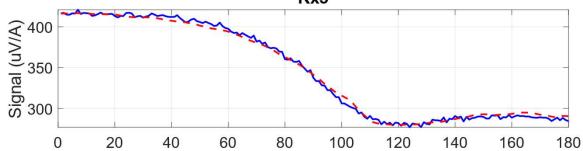
Modelling Inputs



Predicted Response

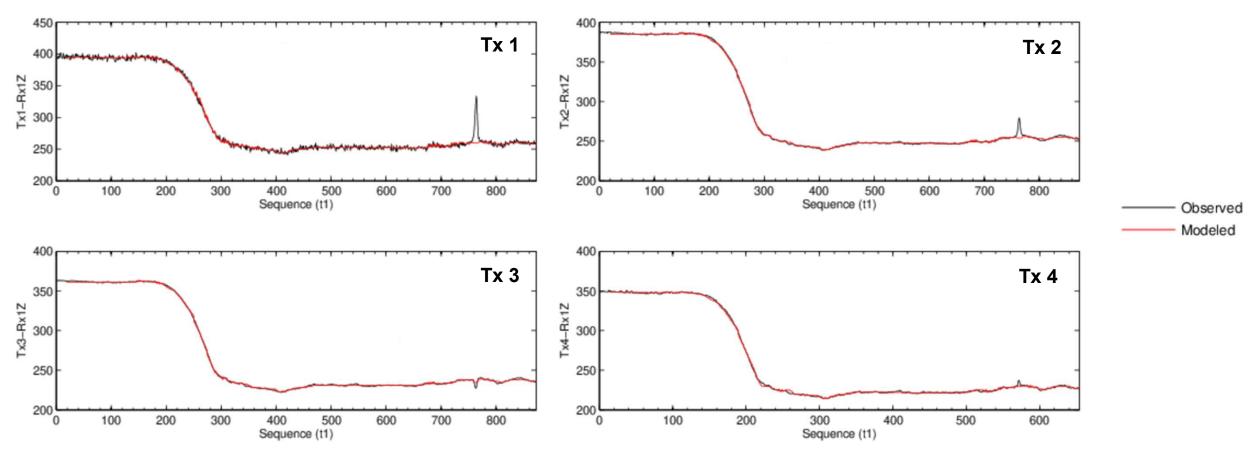






Background signal removal using IE modelling

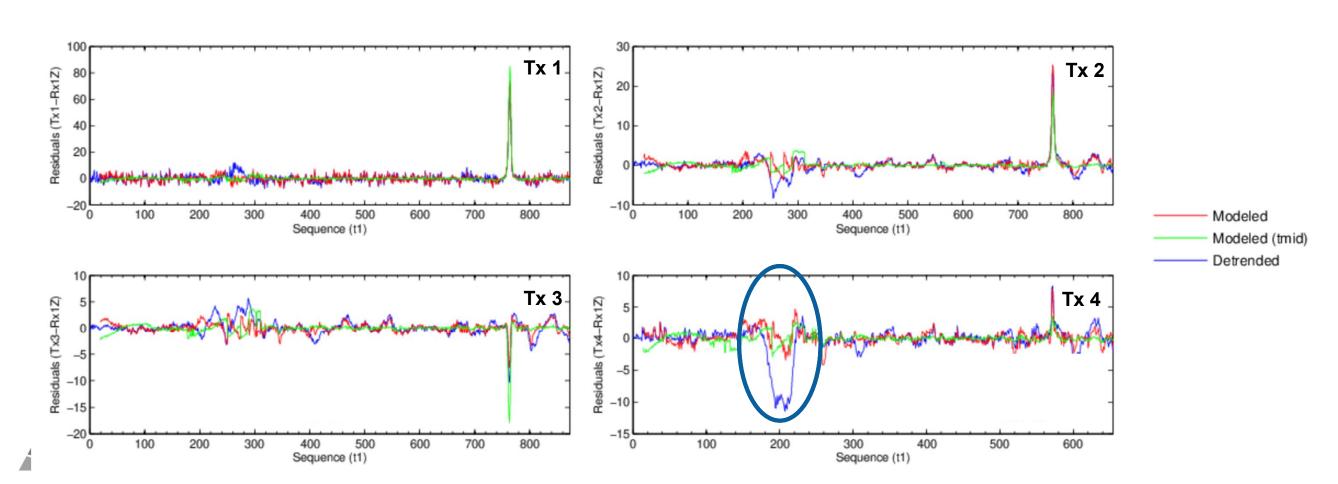
- Line 3, Rx1, Z-comp
- time = 0.19ms





Background signal removal using IE modelling

 Rapid changes in background signal due to variations in sensor altitude and attitude can be more effectively removed using modelling instead of detrend filtering.



Modelling scattered responses

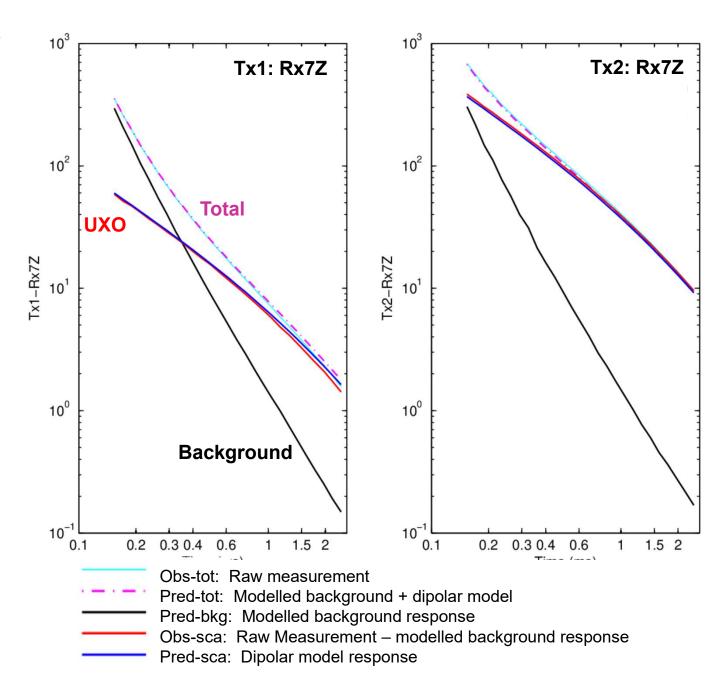
- Integral equation modelling used to study scattered responses in a conductive medium – e.g., spheroids in a layered medium
- Interaction effects are very subtle if they are present
- Theoretically after approximately 0.1 ms the UW response well approximated as a superposition of dipolar target response and a conductive background response

 Right: Layered modelling compared to UltraTEMA measurements at Sequim Bay









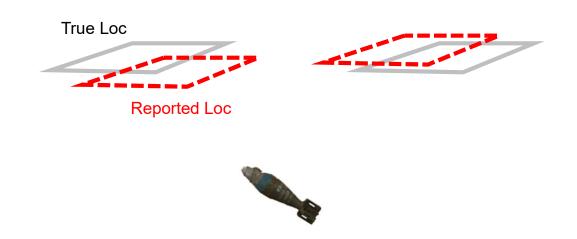
Mitigating sensor positional uncertainty

 Relative positional errors between adjacent survey lines can lead to an erroneous inversion and subsequent misinterpretation



JETSP: Joint Estimation of target and Survey/sensing Parameters

Explicitly account for sensor positioning errors as unknown perturbations that are to be solved



IMLI: Independent Model Location Inversion

Introduce intermediate steps where each line (or shot location) has an independent model location and orientation, while solving for common polarizabilities for a target.

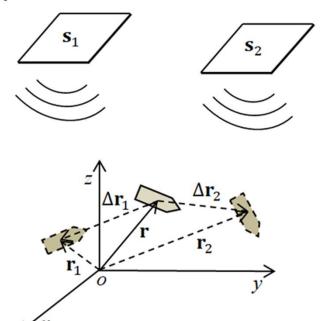






Mitigating sensor positional uncertainty: IMLI

- Break the full dataset into subregions and allow the position and orientation of the item in each subregion to differ
- The principal axis polarizabilities $\beta(t)$ are shared across the regions





Minimize the function

$$\|\boldsymbol{d}_{RT}(\boldsymbol{x},t)-\boldsymbol{s}_{RT}(\boldsymbol{x},\boldsymbol{\beta}(t),\boldsymbol{\theta},\boldsymbol{x}_{\boldsymbol{\beta}})\|$$

by solving for

$$\boldsymbol{\beta}(t), \boldsymbol{\theta}, \boldsymbol{x}_{\boldsymbol{\beta}}$$



IMLI method

Break region into N subregions: x_n , d_n

Minimize the function

$$\sum_{n} \|\boldsymbol{d}_{n}(\boldsymbol{x}_{n},t) - \boldsymbol{s}_{RT}(\boldsymbol{x}_{n},\boldsymbol{\beta}(t),\boldsymbol{\theta}_{n},\boldsymbol{x}_{\boldsymbol{\beta}n})\|$$

by solving for

$$\boldsymbol{\beta}(t), \boldsymbol{\theta}_n, \boldsymbol{x}_{\boldsymbol{\beta}n}$$

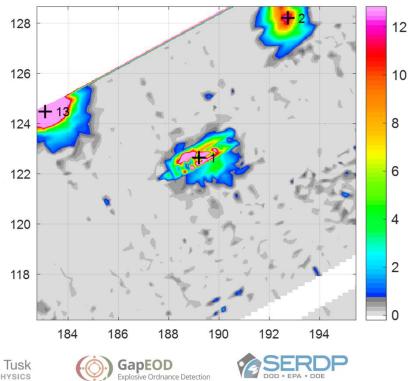


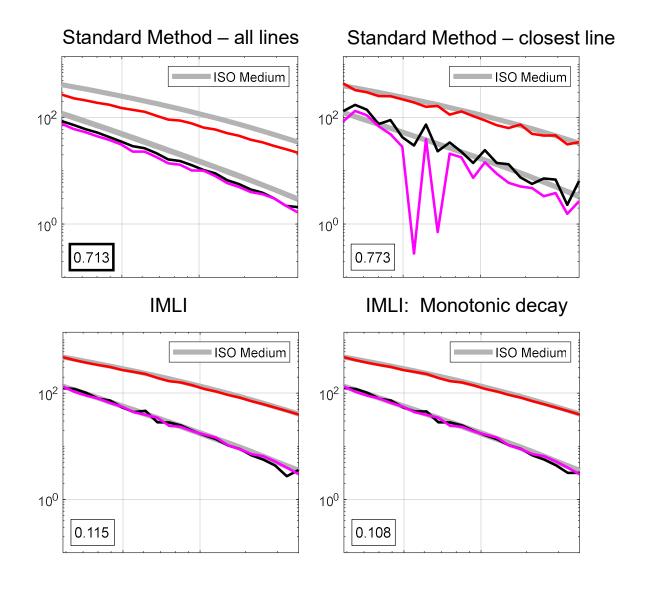




Mitigating sensor positional uncertainty: IMLI

- Medium ISO in Calibration lane
- Data fit for standard is 0.86
- Data fit for IMLI is 0.95

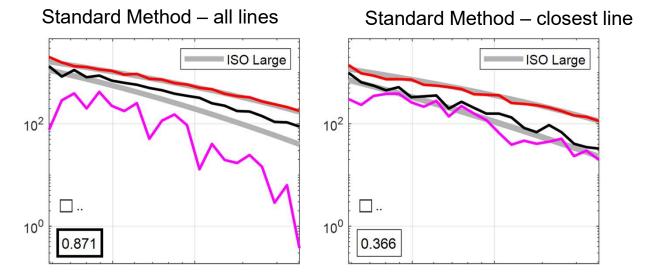


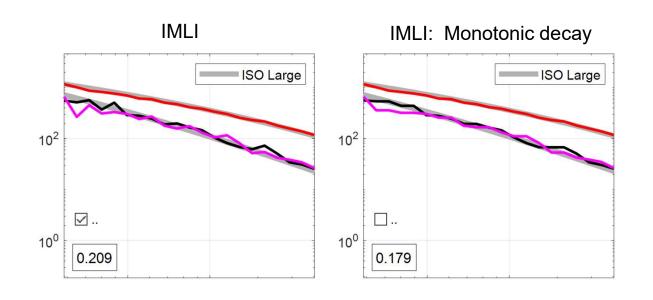




Mitigating sensor positional uncertainty: IMLI

- Large ISO in Calibration lane
- Increased standoff: 1.75m
- Error in relative positioning results in inability to recover all polarizabilities accurately.
- Using only the closest line does recover the polarizabilities, but are "noisy"
- Best fit to Large ISO pols occur when using all lines and accounting for positioning errors.











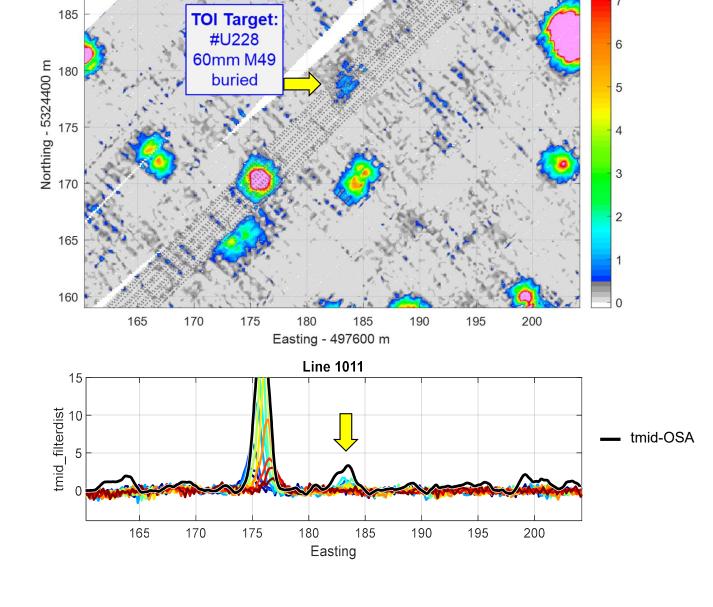
Enhancing Target Detectability

- Exploring Synthetic Aperture (SA) type methods for improving detection performance
- By reciprocity principle, SA can be applied as synthetic transmitting or receiving
- Determine optimal weights to improve signal

$$\underline{d_{\xi i,SA}(t)} = \sum_{l=1}^{L} w_{\psi,l} d_{\xi \psi,il}(t) = \mathbf{B}_{\xi}^{\mathrm{T}}(\mathbf{r}, \mathbf{r}_{i}) P(t) \mathbf{T}_{\psi,SA}$$

$$\mathbf{T}_{\psi,SA} = \sum_{l=1}^{L} w_{\psi,l} \, \mathbf{T}_{\psi}(\mathbf{r}, \mathbf{r}_{l})$$

 Continuing to investigate different approaches and weighting schemes to further boost SNR.



Ch: tmid_filterdist - Inclusive RxC: Z

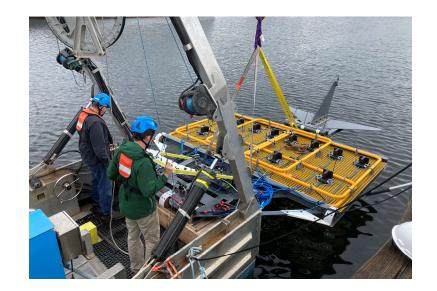


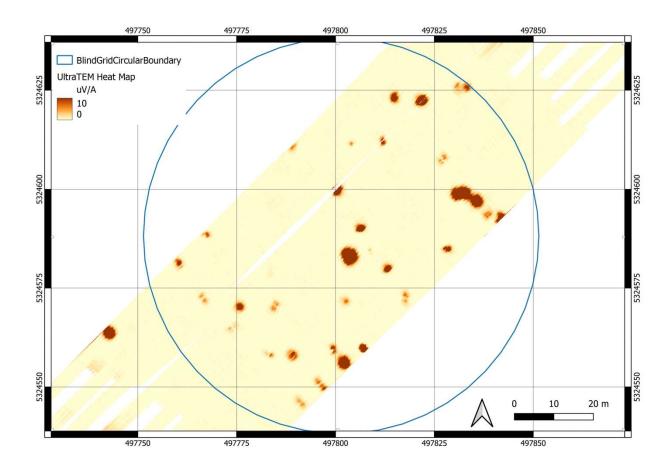




2021 Sequim Bay Test

- Initial testing
- By matching three recovered polarizabilities against the ordnance (UltraTEM) library.
- 27 objects were classified as being most likely to be a UXO
- 10 objects were classified as being most likely to be clutter.





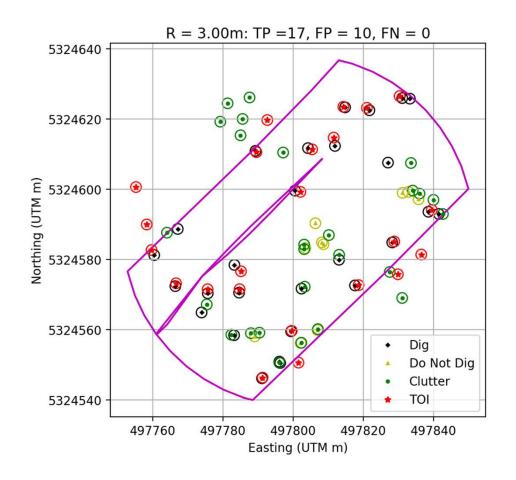


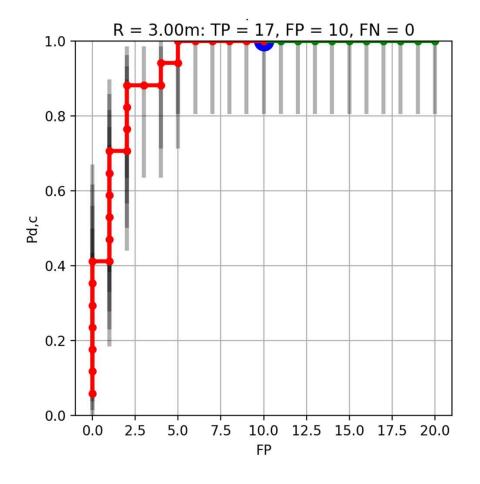




2021 Sequim Bay Blind-Grid results

18	Clutter
1	155m Howitzer M107
3	105mm M60
1	105mm HEAT
4	81mm M821 finned
6	81mm M889A1
2	60mm M49





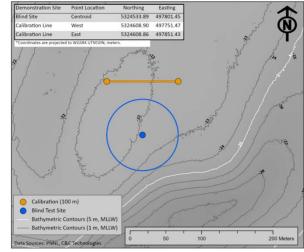






Sequim Bay 2022 Demonstration

Three data sets acquired





90 Hz base-frequency lowest achievable altitude

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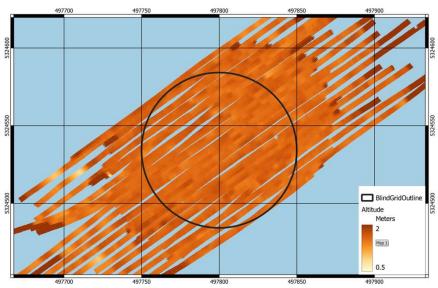
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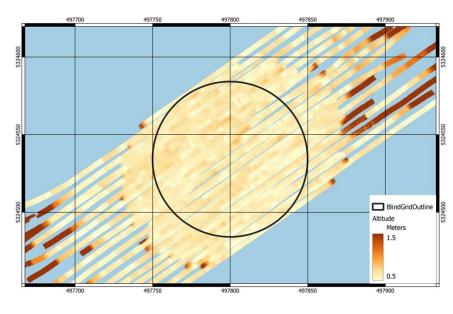
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90 Hz base-frequency 1.5 m survey altitude

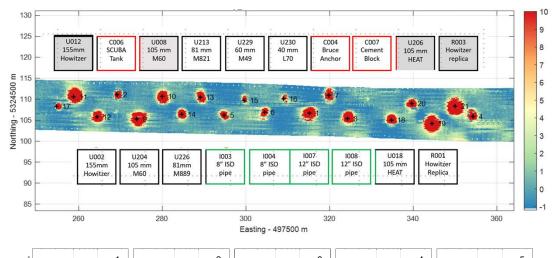


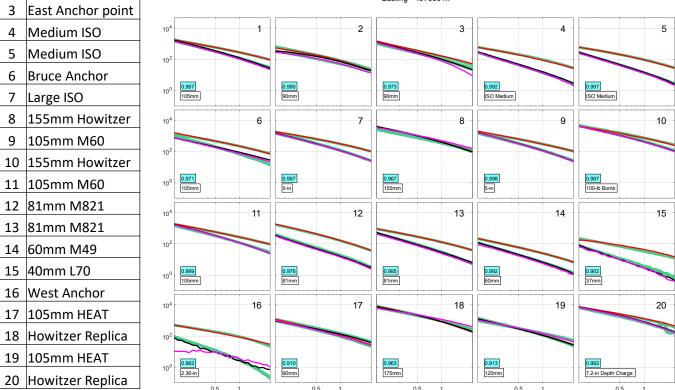
30 Hz base-frequency lowest achievable altitude



Sequim Bay 2022: Calibration Lane



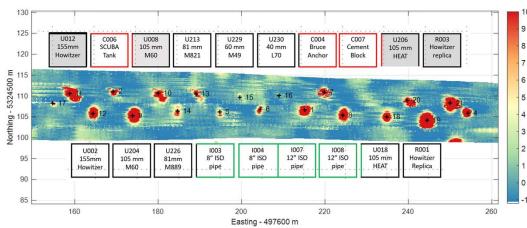


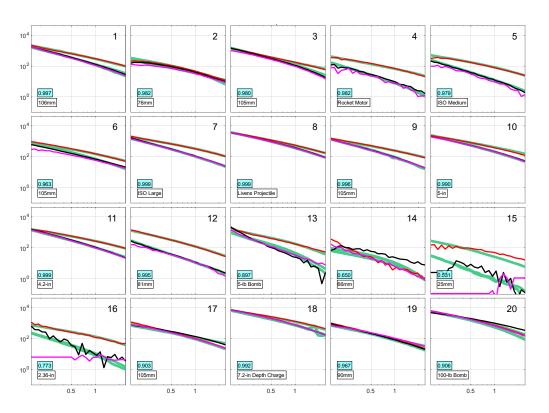


Large ISO

Scuba Tank

1 to 1.25 m altitude



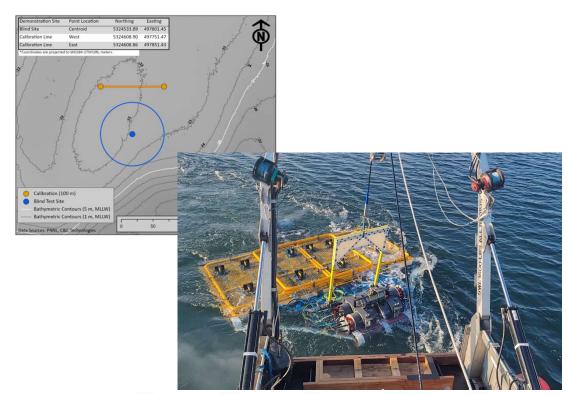


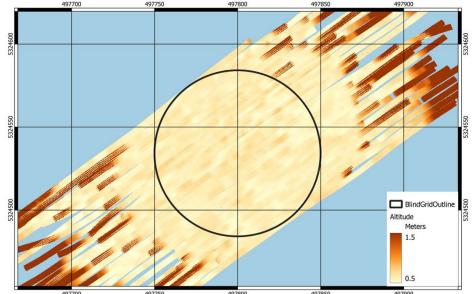
Sequim Bay 2022 Demonstration

Only results from the 90 Hz base-frequency, lowest achievable altitude diglist has been scored.

From Program Office:

- At the demonstrator stop dig point, UltraTEMA successfully detected and classified all TOI with 5 false alarms.
- Use of the optimum stop dig point would have resulted in only 2 false alarms at the Pd,c = 100% point on the ROC curve.
- Geolocation differences between PNNL ground truth and UltraTEMA positions were significantly larger than in 2021, with a 3.5 m halo required for best performance.











Summary

- Developed a full IE technique to compute the TEM response for an arbitrarily oriented sensor in a multi-layered medium.
 - Conductive background responses are correlated with survey parameters, can obscure
 or distort target responses, and can be removed via modeling the UW environment as
 multiple layers.
 - The impacts of the conductive sea-water on the scattered fields from a buried metallic object are negligible within the time range of interest. Terrestrial EMI modeling techniques and methods can be utilized for marine detection and characterization.
- Developed an inversion methods to account for the errors in sensor positioning.
- Developing methods that can enhance target responses
- Results at Sequim Bay showed that marine EMI sensing has considerable potential to be deployed as a practical and effective AGC tool.







